國立清華大學 105 學年度碩士班考試入學試題

系所班組別:工程與系統科學系 乙組(0525)

考試科目 (代碼): 熱傳學 (2504)

- 1. Please describe the terms or answer the question briefly (20%)
 - (a) Fourier's law of heat conduction
 - (b) Newton's law of cooling
 - (c) Stefan-Boltzmann law of thermal radiation
 - (e) Show that, for an ideal gas, the volumetric thermal expansion coefficient (β) at a given temperature (T) is equal to 1/T. Hint: β is defined as:

$$\beta = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_{P}$$

- 2. Considering a thin micro-electronic component mounted on a thick aluminum substrate with epoxy joint. The component and substrate are each 50 mm a side and their exposed surfaces are cooled by a dielectric fluid at 25 °C with heat transfer coefficient of 1000 W/m²K. The thickness and the thermal conductivity for the aluminum substrate are 8 mm and 240 W/mK, respectively. The thermal resistance due to the epoxy joint (R"_{t,c})is estimated to be 0.9×10⁻⁴ m²K/W. If the maximum allowable temperature for the electronic component is 85 °C, please determine the maximum possible power generated by the micro-electronic component. (20%)
- 3. A semi-infinite plane wall is initially at temperature T₁ and for t≥ 0 the plane surface at x =0 is subjected to a fluid flow at temperature T₀ and heat transfer coefficient h . Determine the transient temperature distribution in the wall. Hint: You may use the Laplace transform table given for your solution.(20%)

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- 4. Considering fully-developed internal flow with a mass flow rate W (kg/s) and inlet temperature T_{in} (K) in a circular pipe with diameter D (m) and length L (m). (a) Please determine the mean temperature of the fluid as a function of distance from the tube inlet (x), if the channel wall is kept at uniform temperature T_s (K). In the fully-developed region, the heat transfer coefficient is determined to be h (W/m²K) and the specific heat of the fluid is Cp (J/kgK).
 - (b) Please also show that the total heat transfer rate from the channel wall to the fluid may be expressed as:

 $q = h \pi DL \Delta T_{lm}$

where ΔT_{lm} is the log-mean temperature difference defined as:

$$\Delta T_{lm} = (\Delta T_e - \Delta T_i) / \ln (\Delta T_e / \Delta T_i)$$

 $\Delta T_i = T_s - T_{in}$; $\Delta T_e = T_s - T_e$. T_e is fluid temperature at the channel exit. (20%)

5. A counter flow, concentric tube heat exchanger is designed to heat water with a 0.2 kg/s flow rate from 35°C to some temperature using hot oil with a flow rate of 0.1 kg/s, which is supplied to the annulus at 100 °C and discharged at 60 °C. The thin-walled inner tube has a diameter of 25 mm, and the heat transfer coefficient for the oil side is determined to be 40 W/m²K. Please determine (a) the total heat transfer rate, (b) the overall heat transfer coefficient, and (c) the length of the heat exchanger. (20%)

Hint: Use an appropriate correlation in the appendix below to determine the heat transfer coefficient for convection inside the inner tube.

The water properties are given as:

 ρ =992 kg/m³ ; Cp=4.18×10³ J/kgK; k_f=0.628 W/mK; μ =6.95×10⁻⁴ kg/ms.

The specific heat for oil is 2131 J/kgK.

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Table 8.4 Summary of convection correlations for flow in a circular tube a.b.e

Correlation		Conditions
$f = 64/Re_D$	(8.19)	Laminar, fully developed
$Nu_D = 4.36$	(8.53)	Laminar, fully developed, uniform q_s''
$Nu_D = 3.66$	(8.55)	Laminar, fully developed, uniform T_s
$\overline{Nu}_D = 3.66 + \frac{0.0668 Gz_D}{1 + 0.04 Gz_D^{2/3}}$	(8.57)	Laminar, thermal entry (or combined entry with $Pr \ge 5$), uniform $T_c(Gz_D = (D/x) Re_D Pr$
$\overline{Nu_D} = \frac{\frac{3.66}{\tanh[2.264 Gz_D^{-1/3} + 1.7 Gz_D^{-2/3}]} + 0.0499 Gz_D \tanh(Gz_D^{-1})}{\tanh(2.432 Pr^{1/6} Gz_D^{-1/6})}$	(8.58)	Laminar, combined entry. $Pr \gtrsim 0.1$, uniform T_c $Gz_D = (D/x) Re_D Pr$
$\frac{1}{\sqrt{f}} = -2.0 \log \left[\frac{e/D}{3.7} + \frac{2.51}{Re_D \sqrt{f}} \right]$	(8.20)	Turbulent, fully developed
$f = (0.790 \ln Re_D - 1.64)^{-2}$	(8.21)	Turbulent, fully developed, smooth walls, $3000 \le Re_D \le 5 \times 10^6$
$Eu_D = 0.023 Re_D^{4/5} Pr^n$	(8.60) ^d	Turbulent, fully developed, $0.6 \le Pr \le 160$, $Re_D \ge 10,000$, $(L/D) \ge 10$, $n = 0.4$ for $T_s > T_m$ and $n = 0.3$ for $T_s < T_m$
$Nu_D = 0.027 Re_D^{4/5} Pr^{1/3} \left(\frac{\mu}{\mu_s}\right)^{0.14}$	(8.61) ^d	Turbulent, fully developed, $0.7 \lesssim Pr \lesssim 16.700$, $Re_D \gtrsim 10.000$, $L/D \gtrsim 10$
$Nu_D = \frac{(f/8)(Re_D - 1000)Pr}{1 + 12.7(f/8)^{1/2}(Pr^{2/3} - 1)}$	(8.62) ⁶	Turbulent, fully developed, $0.5 \le Pr \le 2000$. $3000 \le Re_D \le 5 \times 10^6$. $(L/D) \ge 10$

From: Incropera et al., Principles of Heat and Mass Transfer, 7th Ed.

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Table of Laplace Transform of some functions (From: M. Necati Ozisik, Heat Conduction, 1980)

No	$ar{F}(s)$	F(t)
34	$\frac{(\sqrt{s^2 + a^2} - s)^v}{\sqrt{s^2 + a^2}} (v > -1)$	$a^{v}J_{v}(at)$
35	$\frac{(s - \sqrt{s^2 - a^2})^v}{\sqrt{s^2 - a^2}} (v > -1)$	$a^{v}I_{v}(at)$
36	$\frac{1}{s}e^{-ks}$	u(t-k)
37	$\frac{1}{s^2}e^{-ks}$	(t-k)u(t-k)
38	$\frac{1}{s}e^{-k/s}$	$J_0(2\sqrt{kt})$
39	$\frac{1}{s^{\mu}}e^{-k/s}\left(\mu>0\right)$	$\left(\frac{t}{k}\right)^{(\mu-1)/2}J_{\mu-1}(2\sqrt{kt})$
40	$\frac{1}{s^{\mu}}e^{-k/s}\left(\mu>0\right)$	$\left(\frac{t}{k}\right)^{(\mu-1)/2}I_{\mu-1}(2\sqrt{kt})$
41	$e^{-k\sqrt{s}} (k > 0)$	$\frac{k}{2\sqrt{\pi t^3}} \exp\left(-\frac{k^2}{4t}\right)$
42	$\frac{1}{s}e^{-k\sqrt{s}}(k\geq 0)$	$\operatorname{erfc} \frac{k}{2\sqrt{t}}$
43	$\frac{1}{\sqrt{s}}e^{-k\sqrt{s}} \ (k \ge 0)$	$\frac{1}{\sqrt{\pi t}} \exp\left(-\frac{k^2}{4t}\right)$
44	$\frac{1}{s^{3/2}}e^{-k\sqrt{s}} \ (k\geq 0)$	$2\sqrt{\frac{t}{\pi}}\exp\left(-\frac{k^2}{4t}\right) - k\operatorname{erfc}\frac{k}{2\sqrt{t}}$
		$= 2\sqrt{t} i \operatorname{erfc} \frac{k}{2\sqrt{t}}$
45	$\frac{1}{s^{1+n/2}}e^{-k\sqrt{s}} (n=0,1,2,\ldots,k\geq 0)$	$(4t)^{n/2}i^n \operatorname{erfc} \frac{k}{2\sqrt{t}}$
46	$\frac{e^{-k\sqrt{s}}}{a+\sqrt{s}}(k\geq 0)$	$\frac{1}{\sqrt{\pi t}} \exp\left(-\frac{k^2}{4t}\right) - ae^{ak}e^{a^2t}$
		$\times \operatorname{erfc}\left(a\sqrt{t} + \frac{k}{2\sqrt{t}}\right)$
47	$\frac{e^{-k\sqrt{s}}}{\sqrt{s}(a+\sqrt{s})}(k\geq 0)$	$e^{ak}e^{a^{2}t}\operatorname{erfc}\left(a\sqrt{t}+\frac{k}{2\sqrt{t}}\right)$