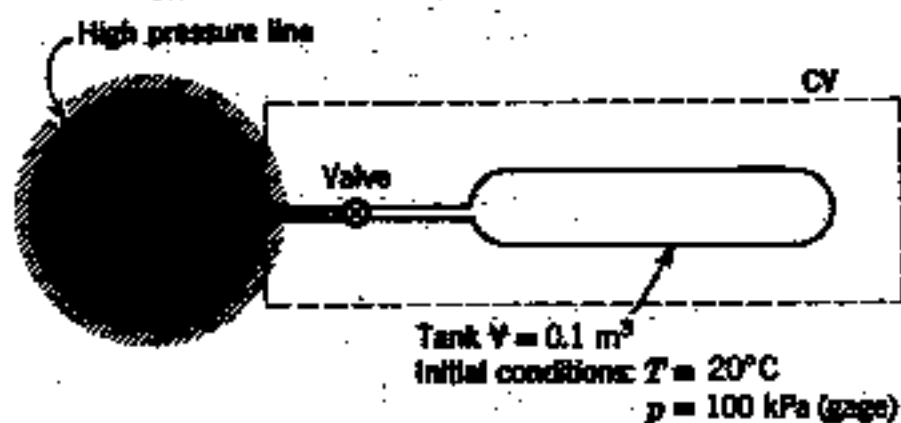


prob. 1  
25 points

A tank of  $0.1 \text{ m}^3$  volume is connected to a high-pressure air line; both line and tank are initially at a uniform temperature of  $20^\circ\text{C}$ . The initial tank gage pressure is  $100 \text{ kPa}$ . The absolute line pressure is  $2.0 \text{ MPa}$ ; the line is large enough so that its temperature and pressure may be assumed constant. The tank temperature is monitored by a fast-response thermocouple. At the instant after the valve is opened, the tank temperature rises at the rate of  $0.05^\circ\text{C/s}$ . Determine the instantaneous flow rate of air into the tank if heat transfer is neglected.



< energy equation:  $\dot{Q} - \dot{W}_s - \dot{W}_{\text{shear}} - \dot{W}_{\text{other}} = \frac{\partial}{\partial t} \int_{CV} e \rho dV + \int_{CS} (e + pV) \rho \hat{V} \cdot d\hat{A}$ ,

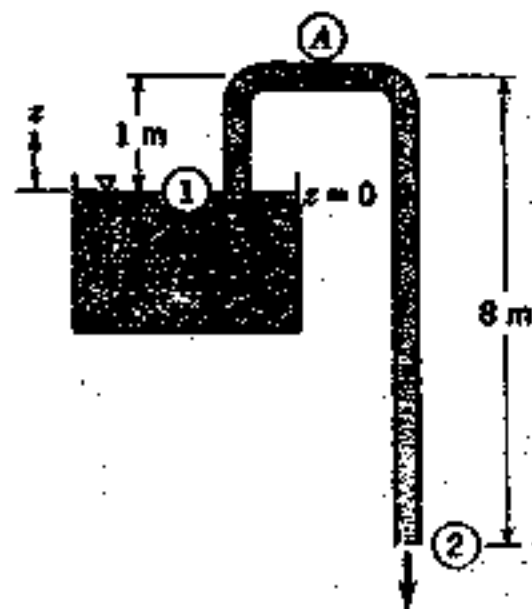
$e = u + \frac{V^2}{2} + gz$ ;

Ideal gas law,  $p = \rho RT$ ,  $du = C_v dT$ ,  $R = 287 \frac{\text{N}\cdot\text{m}}{\text{kg}\cdot\text{K}}$  for air,

continuity equation:  $0 = \frac{\partial}{\partial t} \int_{CV} \rho dV + \int_{CS} \rho \hat{V} \cdot d\hat{A}$ ,  $C_v = 717 \frac{\text{N}\cdot\text{m}}{\text{kg}\cdot\text{K}}$  for air >

prob. 2  
25 points

A U-tube acts as a water siphon. The bend in the tube is  $1 \text{ m}$  above the water surface; the tube outlet is  $7 \text{ m}$  below the water surface. The fluid issues from the bottom of the siphon as a free jet at atmospheric pressure. If the flow is frictionless as a first approximation, determine (after listing the necessary assumptions) the speed of the free jet and the absolute pressure of the fluid in the bend.



<  $P_{\text{atm}} = 1.01 \times 10^5 \frac{\text{N}}{\text{m}^2}$ ;  $\rho_{\text{H}_2\text{O}} = 999 \frac{\text{kg}}{\text{m}^3}$ ;  $g = 9.81 \frac{\text{m}}{\text{s}^2}$  >

Bernoulli's equation:  $\frac{p}{\rho} + \frac{V^2}{2} + gz = \text{constant}$

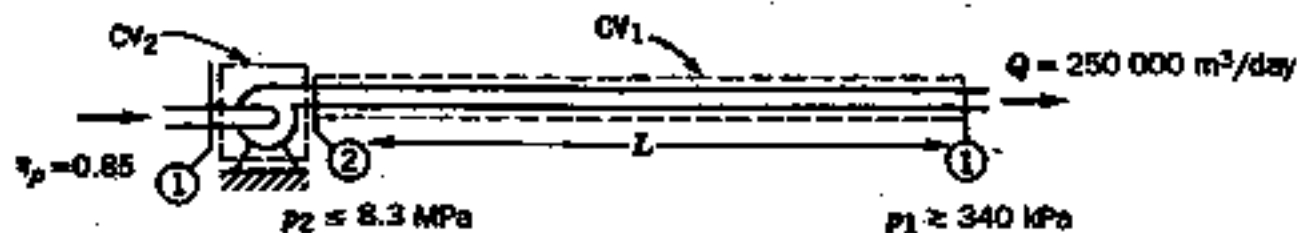
prob. 3  
2.5 points

Consider the flow field given by  $\psi = ax^2 - ay^2$ , where  $a = 3 \text{ s}^{-1}$ . Show that the flow is irrotational. Determine the velocity potential for this flow.

$$\langle \nabla \times \hat{V} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ u & v & w \end{vmatrix} ; \text{Cauchy-Riemann equation, } \begin{aligned} u &= \frac{\partial \psi}{\partial y} = -\frac{\partial \phi}{\partial x} \\ v &= -\frac{\partial \psi}{\partial x} = -\frac{\partial \phi}{\partial y} \end{aligned} \rangle$$

prob. 4  
2.5 points

Crude oil flows through a level section of the Alaskan pipeline at a rate of 250 thousand cubic meters per day. The pipe inside diameter is 1200 mm; its roughness is equivalent to that of galvanized iron. The maximum allowable pressure is 8.3 MPa; the minimum pressure required to keep dissolved gases in solution in the crude oil is 340 kPa. The crude oil has  $SG = 0.93$ ; its viscosity at the pumping temperature of  $60^\circ\text{C}$  is  $\mu = 0.017 \text{ N}\cdot\text{s}/\text{m}^2$ . For these conditions, determine the maximum possible spacing between pumping stations. If the pump efficiency is 85 percent, determine the power that must be supplied at each pumping station.



$$\left\langle \left( \frac{p_2}{\rho} + \alpha_2 \frac{\bar{V}_2^2}{2} + g z_2 \right) - \left( \frac{p_1}{\rho} + \alpha_1 \frac{\bar{V}_1^2}{2} + g z_1 \right) = h_{\text{net}} ; h_{\text{net}} = h_e + h_m = f \frac{L}{D} \frac{\bar{V}^2}{2} + K \frac{\bar{V}^2}{2} \right\rangle$$

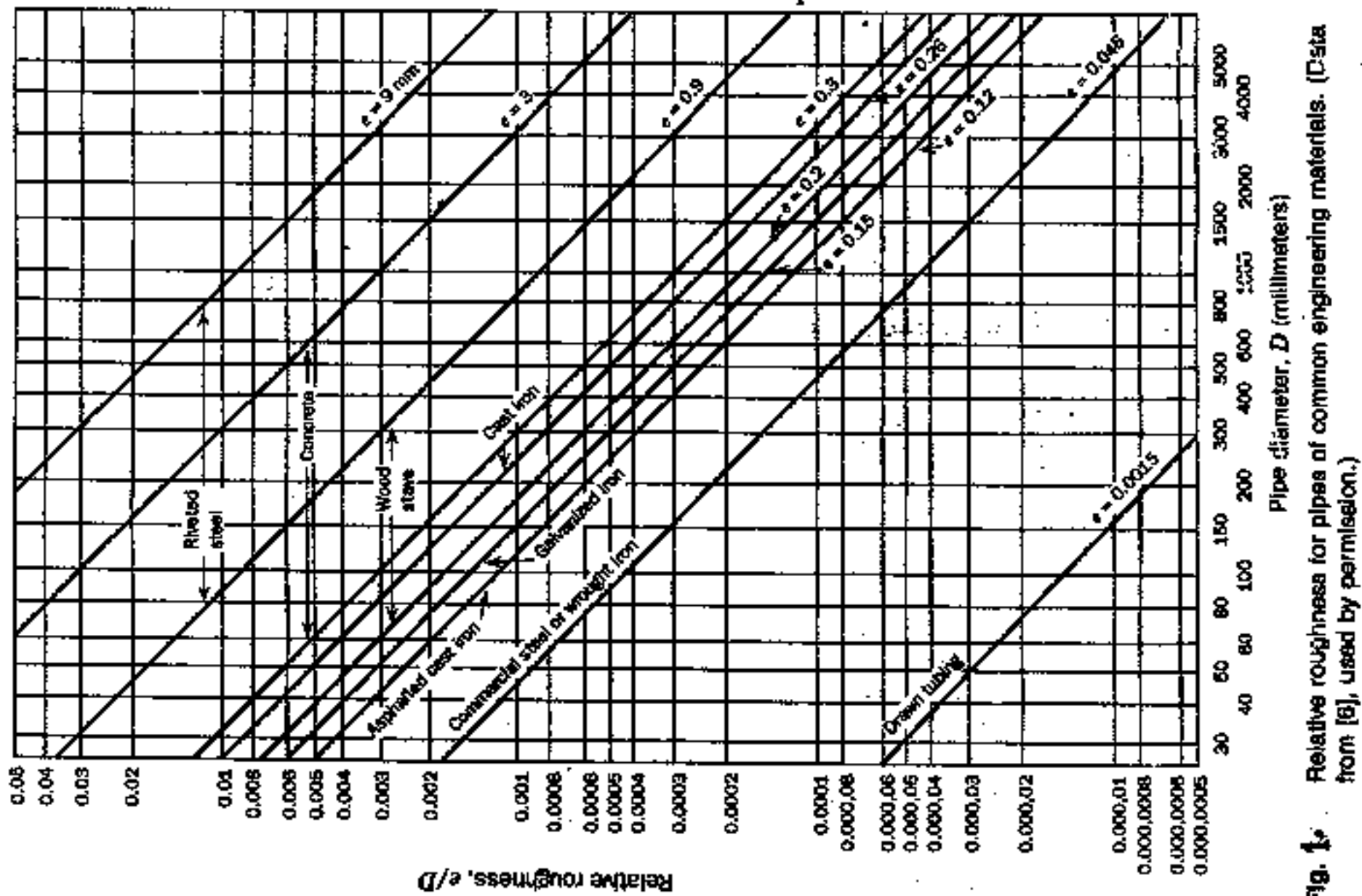


Fig. 1. Relative roughness for pipes of common engineering materials. (Data from [6], used by permission.)

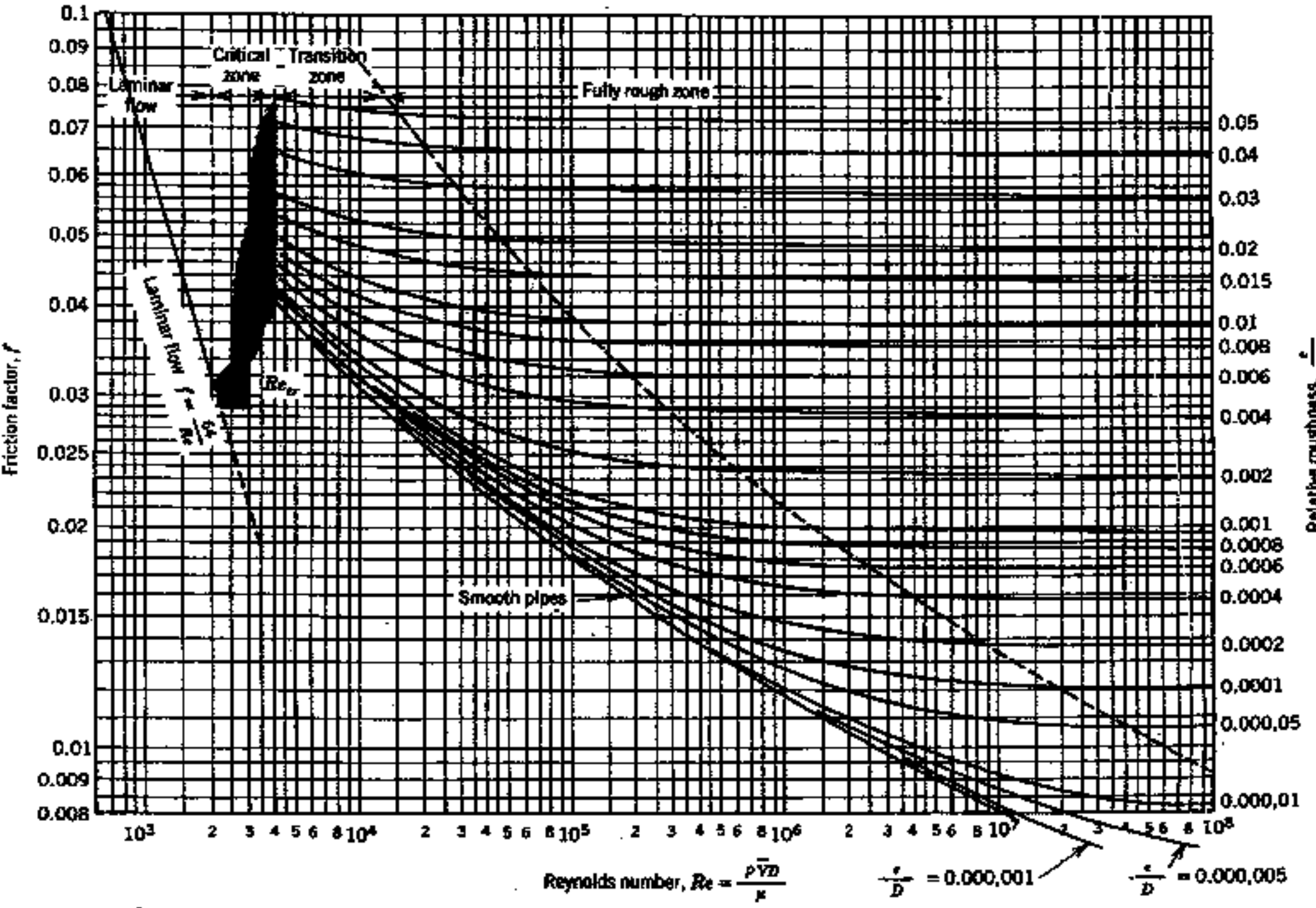


Fig. 2. Friction factor for fully developed flow in circular pipes. (Data from [6], used by permission.)